

# Lattice Boltzmann method for the simulations of miscible gases

Lucien VIENNE<sup>1,a</sup>, Simon MARIÉ<sup>1,b</sup>, Francesco GRASSO<sup>1,c</sup>



<sup>1</sup>Laboratoire DynFluid, Conservatoire National des Arts et Métiers, France <sup>a</sup>PhD student, <sup>b</sup>Assistant professor, <sup>c</sup>Professor

#### Abstract

The model proposed here is derived from an alternative theory of multicomponent fluid diffusion by Kerkhof [1] based on an expansion of the legacy theory of Hirschfelder, Curtiss and Bird [2]. In contrast with the previous lattice Boltzmann models, the diffusion force is directly added to the momentum equation through a Guo's forcing scheme [3]. In addition the corresponding transport coefficients, viscosity and diffusion coefficients for each species, are computed according to the molecular proprieties of the components. Then some numerical simulations are presented for validation purposes.

# A new multicomponent lattice Boltzmann model

The  $\sigma$  superscript denotes different fluid components by specifying  $\sigma = 1, 2, ..., N$  with N being the total number of the components. For simplicity, the components are supposed to have the same molar weight.



$$f_{\alpha}^{\sigma}\left(\mathbf{x}+\mathbf{e}_{\alpha}\delta_{t},t+\delta_{t}\right)=f_{\alpha}^{\sigma}\left(\mathbf{x},t\right)-\frac{1}{\tau^{\sigma}}\left[f_{\alpha}^{\sigma}\left(\mathbf{x},t\right)-f_{\alpha}^{\sigma(eq)}\left(\mathbf{x},t\right)\right]+S_{\alpha}^{\sigma}$$

Where  $f_{\alpha}^{\sigma(eq)}$  is the equilibrium distribution functions of each fluid species:

$$f_{\alpha}^{\sigma(eq)} = \rho^{\sigma} \omega_{\alpha} \left[ 1 + \frac{\mathbf{u}^{\sigma} \cdot \mathbf{e}_{\alpha}}{c_s^2} + \frac{(\mathbf{u}^{\sigma} \cdot \mathbf{e}_{\alpha})^2}{2c_s^4} - \frac{\mathbf{u}^{\sigma} \cdot \mathbf{u}^{\sigma}}{2c_s^2} \right]$$

And  $S^{\sigma}_{\alpha}$  is the source term from Guo forcing scheme where  $\mathcal{F}^{\sigma}$  is the total force acting on the  $\sigma$ th component:

$$S_{\alpha}^{\sigma} = (1 - \frac{\delta_t}{2\tau^{\sigma}})\omega_{\alpha} \left[\frac{\mathbf{e}_{\alpha} - \mathbf{u}^{\sigma}}{c_s^2} + \frac{(\mathbf{e}_{\alpha} \cdot \mathbf{u}^{\sigma})\mathbf{e}_{\alpha}}{c_s^4}\right] \cdot \mathcal{F}^{\sigma}$$

As a **multi-fluid** approach of the mixture, the density and the momentum of each fluid components are defined as:

$$\mathcal{F}^{\sigma} = \mathcal{F}^{\sigma}_{D} + \mathcal{F}^{\sigma}_{ext}, \quad \text{with } \mathcal{F}^{\sigma}_{D} = -p \sum_{\varsigma=1}^{n} \frac{x_{\sigma} x_{\varsigma}}{\mathcal{D}_{\sigma\varsigma}} (\mathbf{u}^{\sigma} - \mathbf{u}^{\varsigma})$$

A Chapman and Enskog expansion procedure gives the following macroscopic equations for low mach number and isothermal flow:

 $\begin{aligned} \partial_t \rho^{\sigma} + \nabla \cdot (\rho^{\sigma} \mathbf{u}^{\sigma}) &= 0\\ \partial_t (\rho^{\sigma} \mathbf{u}^{\sigma}) + \nabla \cdot (\rho^{\sigma} \mathbf{u}^{\sigma} \otimes \mathbf{u}^{\sigma}) &= -\nabla p^{\sigma} + \nabla \cdot \left[ \mu^{\sigma} \left( \nabla \mathbf{u}^{\sigma} + (\nabla \mathbf{u}^{\sigma})^T \right) \right] \\ &- p \sum_{\varsigma=1}^N \frac{x_{\sigma} x_{\varsigma}}{\mathcal{D}_{\sigma\varsigma}} (\mathbf{u}^{\sigma} - \mathbf{u}^{\varsigma}) + \mathcal{F}_{ext}^{\sigma} \end{aligned}$ Where  $p^{\sigma} = \rho^{\sigma} c_s^2$ ,  $p = \sum_{\sigma=1}^N p^{\sigma}$ ,  $\mu^{\sigma} = \rho^{\sigma} c_s^2 (\tau^{\sigma} - \frac{\delta_t}{2})$ 

## Transport coefficients

$$\begin{pmatrix} \mu^{\sigma} \end{pmatrix} = \begin{bmatrix} P_{\sigma\varsigma} \end{bmatrix}^{-1} \begin{pmatrix} 1 \\ \vdots \\ 1 \end{pmatrix}$$

$$P_{\sigma\sigma} = \frac{2}{k_B T} \begin{bmatrix} \frac{4}{5} \Omega_{\sigma}^{(2,2)} + \sum_{\varsigma \neq \sigma}^{N} \frac{x_{\varsigma} 16}{x_{\sigma} 15} \frac{m_{\varsigma}}{(m_{\sigma} + m_{\varsigma})^2} \left( 5m_{\sigma} \Omega_{\sigma\varsigma}^{(1,1)} + \frac{3}{2} m_{\varsigma} \Omega_{\sigma\varsigma}^{(2,2)} \right) \end{bmatrix}$$

$$P_{\sigma\varsigma} = -\frac{2}{k_B T} \begin{bmatrix} \frac{16}{15} \frac{m_{\sigma} m_{\varsigma}}{(m_{\sigma} + m_{\varsigma})^2} \left( 5\Omega_{\sigma\varsigma}^{(1,1)} - \frac{3}{2} \Omega_{\sigma\varsigma}^{(2,2)} \right) \end{bmatrix}$$

$$\mu^{\text{mixture}} = \sum_{\sigma}^{N} \mu^{\sigma}, \quad \mathcal{D}_{\sigma\varsigma} = \frac{3(m_{\sigma} + m_{\varsigma})(k_B T)^2}{16 p m_{\sigma} m_{\varsigma}} \frac{\Omega_{\sigma\varsigma}^{(1,1)}}{\Omega_{\sigma\varsigma}^{(1,1)}}$$

## Limit expression: decay of a sinusoidal density wave

For binary equimolar mixture with negligible convection, the flow dynamics are essentially governed by diffusion and equivalent equations reduce to a diffusion equation. Measured diffusion coefficients is then compared to the theoretical values [4].

$$\rho^{\sigma}(\mathbf{x}, \mathbf{t}) = \rho^{mean} + \delta \sin(\mathbf{k}\mathbf{x}) \exp(-\mathbf{k}^2 \mathcal{D}\mathbf{t})$$

$$\tau = 0.6$$

Where  $k_B$  is the Boltzmann constant, T the temperature,  $m_{\sigma}$  the mass of the component  $\sigma$ ,  $x_{\sigma}$  the mole fraction and  $\Omega$ -integrals have the same definition as in [2] and depend on the temperature and the molecular proprieties based on the Lennard-Jones potential.





#### Perspectives

- Different molar massThree and more species
- More validation test-cases
- Chemical reactions: source/sink terms and temperature

# Simulation of the viscous fingering instability

Macro-scale simulation:  $\Delta x \gg \text{pore length}$ 



Viscous fingering instability occurs when a less viscous fluid displaces a more viscous one.

Pore-scale simulation: $\Delta x < \text{pore length}$ 



 Partial bounce-back [5] :
 f<sup>coll</sup><sub>α</sub> = (1 - n<sub>s</sub>) × Coll + n<sub>s</sub> × f<sub>opp</sub>
 n<sup>σ</sup><sub>s</sub>[i, j] = ν<sup>σ</sup>/(2K + ν<sup>σ</sup>)
 where K is the permeability of
 the medium.

- Diameter of the pores: 16 Lu
- Standard bounce-back with MRT formulation [6]
- Emergence of asymmetric patterns in the mixing zone

## References

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